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(S4) Process and catalyst for producing reactor blend polyolefins.

Polyolefin reactor blends obtained by polymerization of ethylene and higher alpha-olefins in the presence of a catalyst system comprising two or more metallocenes and alumox-

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PROCESS AND CATALYST FOR PRODUCING REACTOR HIEND POLYOLEFINS

The present invention concerns catalyst and process for the polymerization of ethylene and alpha-olefins. More 2 particularly, the invention relates to catalysts and process 3 for producing (co)polyolefin reactor blends of ethylene and 4 ethylene-alpha-olefin copolymers. The invention further 5 relates to a sprocess for producing tailored (co)polyolefins 6 reactor blends through the proper selections of the catalysts 7 . alofathistinvention::.atbancapy tennostation sefis ? -Reactor blends for purposes of this invention are mixtures 9 of two or more polymers of different physical properties 10 (density, melting point, comonomer content, etc.) produced 11 simultaneously in a single polymerization reactor. Catalyst 12 employed in the production of such polymer blends under steady 13 state conditions in one reactor will comprise two or more 14 . distinct catalyst components, one predominately catalyzing the 15 formation of one polymer, the other predominately catalyzing 16 the formation of the other polymer. 17

DESCRIPTION OF THE PRIOR ART

It is known that certain metallocenes such as bis(cyclopentadienyl) titanium and zirconium dialkyls in combination with aluminum alkyl co-catalyst, form homogeneous catalyst systems useful for the polymerization of ethylene. German Patent Application 2,608,863 discloses the use of a catalyst system for the polymerization of ethylene consisting of bis(cyclopentadienyl) titanium dialkyl, aluminum trialkyl and water. German Patent Application 2,608,933 discloses an ethylene polymerization catalyst system consisting of (1) zirconium metallocenes of the general formula $(cyclopentadienyl)_n ZrY_{4-n}$, wherein n stands for a number in the range of 1 to 4, Y for R, CH2AlR2, CH2CH2AlR2 and CH2CH(AIR2)2 wherein R stands for alkyl or metallo alkyl, (2) an alumiunum trialkyl cocatalyst and (3) water. European Patent Appln. No. 0035242 discloses a process for preparing ethylene and atactic propylene polymers in the

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presence of a halogen-free Ziegler catalyst system of (1) cyclopentadienyl compound of the formula (cyclopentadienyl) MeY4-n in which n is an integer from 1 to 4. Me is a transition metal, especially zirconium, and Y is either hydrogen, a C1-C5 alkyl or metallo alkyl group or a compound having the following general formula: CH2AlR2, CH2CH2AlR2 and CH2CH(AlR2)2 in which R represents a C1-C5 alkyl or metallo alkyl group, and (2) an alumoxane.

The above disclosures demonstrate the usefulness of certain metallocenes in combination with certain aluminum compounds for the polymerization of ethylene and particularly polymerization at a high activity rates. The references neither disclose polyethylene/copolyethylene-alpha-olefin reactor blends nor methods of producing such reactor blends.

In "Molecular Weight Distribution And Stereoregularity Of Polypropylenes Obtained With $Ti(OC_4H_9)_4/Al(C_2H_5)_3$ Catalyst System"; Polymer, Pg. 469-471, 1981, Vol. 22, April, Doi, et al disclose propylene polymerization with a catalyst which at about $4l^OC$ obtains a soluble catalyst and insoluble catalyst fraction, one with "homogeneous catalytic centres" and the other with "heterogeneous catalytic centres". The polymerization at that temperature obtains polypropylene having a bimodal molecular weight distribution.

It is also known to produce polymer blends by polymerizing two or more polymerizable materials in two or more reactors arranged in series. In accordance with such methods, a polymerizate is produced in a first reactor which first polymerizate is passed to a second reactor wherein a second polymerizate is produced thereby obtaining a blend of the first and second polymerizates.

It is highly desirable to be able to readily and simply produce blends in a single reactor during which polyethylene and copolyethylene-alpha-olefins are produced simultaneously. Not only is a significant reduction in energy costs obtained, but one obtains a uniform blending of the polymers and one can simply "tailor" the polymers with respect to molecular weights,

weight fraction and the like to obtain blends evidencingoutstanding properties.

In view of the foregoing problems, it would be highly desirable to provide a polymerization catalyst system of sufficient activity to produce high quality blends of ethylene-alpha olefin polymers. It is furthermore highly desirable to be able to produce the blends of ethylene-alpha olefin polymers directly in a single reactor.

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The present invention provides a process for producing (co)polyolefin reactor blends comprising polyethylene and copolyethylene-alpha-olefins. The reactor blends are obtained directly during a single polymerization process, i.e., the blends of this invention are obtained in a single reactor by simultaneously polymerizing ethylene and copolymerizing ethylene with an alpha-olefin thereby eliminating expensive blending operations. The invention furthermore provides a catalyst system for the polymerization of ethylene and ethylene copolymers simultaneously to provide polyethylene blends. The process of producing reactor blends in accordance with this invention can be employed in conjunction with other prior art blending techniques, for example the reactor blends produced in a first reactor can be subjected to further blending in a second stage by use of a series of reactors.

Accordingly, there is provided a catalyst system for the polymerization of reactor blends of polyethylene with ethylene-alpha-olefin copolymers; said catalyst system comprising (a) at least two different metallocenes and (b) an alumoxane. The metallocenes employed in this invention are organometallic coordination compounds which are cyclopentadienyl derivatives of a transition metal of Groups 4b, 5b and 6b and include mono, di and tricyclopentadienyls and their derivatives of the transition metal. The metallocenes can be represented by the general formula

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 $(C_5R'_m)_pR''_s(C_5R'_m)MeQ_{3-p}$ or $R''_s(C_5R'_m)MeQ'_s$ 1 wherein (C_R'm) is a cyclopentadienyl or substituted 2 cyclopentadienyl, each R'., which can be the same or different, is hydrogen or a hydrocarbyl radical such as alkyl, alkenyl, aryl, alkylaryl, or arylalkyl radical having from 1 to 20 carbon atons or two R! substituents together form a fused Ci-Cering, R" is a C1-C1 alkylene radical, a dialkyl germanium or silicone, or an alkyl phosphine or amine radical bridging two $(C_5R_m^1)$ rings, Q is a hydrocarbon radical such as aryl, alkyl, alkenyl, alkylaryl, or arylalkyl radical having 10 from 1 to 20 carbon atoms or halogen and each Q can be the same or 11 different, Q' is an alkylidene radical having from 1 to about 12 20 carbon atoms, Me is a transition metal of Group 4b, 5b, 6b 13 of the Periodic Table (Chemical Rubber Company's Handbook of 14 Chemistry & Physics, 48th Edition), s is 0 or 1, p is 0, 1 or 15 2; when p = 0, s = 0; m is 4 when s is 1 and m is 5 when s is 0. 16

The ratios of one metallocene to the second metallocene will be a function of both the chemical composition of the metallocenes as well as the blend being tailored; accordingly, the ratio of the two metallocenes can vary greatly and, hence, is limited only for the purpose of producing the blends.

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The present invention also provides a process for producing polyolefin reactor blends. The process comprises polymerizing ethylene and higher alpha-olefins in the presence of the catalyst system described above.

DETAILED DESCRIPTION OF THE INVENTION

The present invention is directed towards a catalytic process for the polymerization of ethylene and one or more alpha-olefins to polyethylene-copolyethylene-alpha-olefin reactor blends. The polymers are intended for fabrication into articles by extrusion, injection molding, thermoforming, rotational molding, and the like. In particular, the polymer blends of this invention are blends of polyethylenes such as high density polyethylene (HDPE) and linear low density polyethylene (LLDPE) and with copolyethylene higher alpha-olefins having from 3 to about 10 carbon atoms and

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preferably 4 to 8 carbon atoms. Illustrative of the higher alpha-olefins are propylene, butene-1, hexene-1 and octene-1. Preferably, the alpha-olefin is propylene or butene-1.

In the process of the present invention, ethylene, together with the alpha-olefins, is polymerized in the presence of a homogeneous catalyst system comprising at least two different metallocenes and an alumoxane.

The alumoxanes are well known in the art and are polymeric aluminum compounds which can be represented by the general formulae $(R-Al-0)_n$ which is a cyclic compound and $R(R-Al-0-)_nAlR_2$, which is a linear compound. In the general formula R is a C_1-C_5 alkyl group such as, for example, methyl, ethyl, propyl, butyl and pentyl and n is an integer from 1 to about 20 and preferably from about 1 to about 4. Most preferably, R is methyl and n is 4. Generally, in the preparation of alumoxanes from, for example, aluminum trimethyl and water, a mixture of the linear and cyclic compounds are obtained.

The alumoxane can be prepared in various ways. Preferably, they are prepared by contacting water with solution of aluminum trialkyl, such as, for example, aluminum trimethyl, in a suitable organic solvent such as benzene or an aliphatic hydrocarbon. For example, the aluminum alkyl is treated with water in form of a moist solvent or the aluminum alkyl such as aluminum trimethyl can be desirably contacted with a hydrated salt such as hydrated copper sulfate.

Preferably, the alumoxane is prepared in the presence of a hydrated copper sulfate. The method comprises treating a dilute solution of aluminum trimethyl in, for example, toluene, with copper sulfate represented by the general formula CuSO₄.5H₂O. The ratio of copper sulfate to aluminum trimethyl is desirably about 1 mole of copper sulfate for 5 moles of aluminum trimethyl. The reaction is evidenced by the evolution of methane.

The dual metallocene system usefully employed in accordance with this invention are the mono, di and tricyclopentadienyl or substituted cyclopentadienyl metallocenes and preferably the

titanium (IV) and zirconium (IV) metallocenes. The 1 metallocenes are represented by the general formula 2 $(C_5R'_m)_nR''_s(C_5R'_m)MeQ_{3-p}$ and R" (C5R'm) MeQ' wherein (C5R'm) is cyclopentadienyl or substituted cyclopentadienyl, each R' is the same or different and is hydrogen or a hydrocarbyl radical such as alkyl, alkenyl, aryl, alkylaryl, or arylalkyl radicals containing from 1 to 20 carbon atoms or two carbon atoms are joined together to form a C4-C6 ring, R1 is a C1-C4 alkylene radical, a dialkyl germanium or silicone, or an alkyl phosphine or amine radical bridging two (C5R'm) rings, Q is 11 a hydrocarbyl radical such as aryl, alkyl, alkenyl, alkylaryl, 12 or arylalkyl radical having from 1-20 carbon atoms or halogen 13 and can be the same or different, Q' is an alkylidene radical 14 having from 1 to about 20 carbon atoms, s is 0 or 1, p is 0, 1 15 or 2; when p is 0, s is 0, m is 4 when s is 1 and m is 5 when s 16 is O and Me is a Group 4b, 5b or 6b transition metal and most 17 preferably zirconium or titanium. 18 Exemplary hydrocarbyl radicals are methyl, ethyl, propyl, 19

Exemplary hydrocarbyl radicals are methyl, ethyl, propyl, butyl, amyl, isoamyl, hexyl, isobutyl, heptyl, octyl, nonyl, decyl, cetyl, 2-ethylhexyl, phenyl, and the like.

Exemplary alkylene radicals are methylene, ethylene, propylene, and the like.

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Preferred examples of substituent Q are methyl, phenyl or chloride.

Exemplary halogen atoms include chlorine, bromine and iodine and of these halogen atoms, chlorine is preferred.

Exemplary of the alkylidene radicals are methylidene, ethylidene and propylidene.

Preferably the catalyst comprises at least two zirconocenes or at least one titanocene and at least one zirconocene.

Illustrative but non-limiting examples of the titanocenes which can be usefully employed in accordance with this invention are bis(cyclopentadienyl) titanium

- 1 diphenyl, the carbene represented by the formula
- 2 Cp₂Ti=CH₂ · Al(CH₃)₂Cl, and derivatives of this
- 3 reagent such as Cp_Ti=CH2 'Al(CH3)3,
- 4 (Cp₂TiCH₂)₂, Cp₂TiCH₂CH(CH₃)CH₂,
- 5 Cp₂Ti=CHCH₂CH₂, Cp₂Ti=CH₂ AlR'''₂Cl, wherein Cp
- 6 is a cyclopentadienyl or substituted cylopentadienyl

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and R''' is an alkyl, aryl or alkylaryl radical having from 1 1-18 carbon atoms; substituted bis(Cp)Ti(IY) compounds such as 2 bis(indenyl)Ti diphenyl or dichloride, bis(methylcyclopentadienyl)Ti diphenyl or dihalides and other dihalide complexes; dialkyl, trialkyl, tetra-alkyl and penta-alkyl cyclopentadienyl titanium compounds such as bis(1,2-dimethylcyclopentadienyl)Ti diphenyl or dichloride, -=bis(fluorenyl)Ti dichloride, bis(1,2-diethylcyclopentadienyl)Ti diphenyl or dichloride and other dihalide complexes; silicone, phosphine, amine or carbon bridged cyclopentadiene complexes, 10 such as dimethyl silyldicyclopentadienyl titanium diphenyl or 11 dichloride, methyl phosphine dicyclopentadienyl titanium 12 diphenyl or dichloride, methylenedicyclopentadienyl titanium 13 diphenyl or dichloride and other dihalide complexes. 14 Illustrative but non-limiting examples of the zirconocenes 15 which can be usefully employed in accordance with this 16 invention are bis(cyclopentadienyl)zirconium diphenyl, 17 bis(cyclopentadienyl)zirconium dimethyl; the alkyl substituted 18 cyclopentadienes, such as bis(ethyl cyclopentadienyl)zirconium 19 dimethyl, bis $(\beta$ -phenylpropylcyclopentadienyl)zirconium 20 dimethyl, bis(methylcyclopentadienyl)zirconium dimethyl and 21 dihalide complexes of the above; di-alkyl, tri-alkyl, 22 tetra-alkyl, and penta-alkyl cyclopentadienes, such as 23 bis(pentamethylcyclopentadienyl)zirconium dimethyl, bis 24 (1,2-dimethylcyclopentadienyl)zirconium dimethyl, 25 bis(1,3-diethylcyclopentadienyl)zirconium dimethyl and dihalide 26 complexes of the above; silicone, phosphorus, and carbon 27 bridged cyclopentadiene complexes such as 28 dimethylsilyldicyclopentadienyl zirconium dimethyl or dihalide, 29 methylphosphine dicyclopentadienyl zirconium dimethyl or 30 dihalide, and methylene dicyclopentadienyl zirconium dimethyl 31 or dihalide, carbenes represented by the formulae 32 $Cp_2Zr=CH_2P(C_6H_5)_2CH_3$, and derivatives of these 33 compounds such as Cp_ZrCH_CH(CH3)CH2. 34 The ratio of aluminum in the alumoxane to total metal in 35 the metallocenes can be in the range of 0.5:1 to 36

5:1 to

10⁵:], and preferably

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ratio of the metallocenes can vary over a wide range and in accordance with this invention the molar ratios are controlled by the product polymer blend desired.

The reactivity ratios of the metallocenes in general are obtained by methods well known such as, for example, as described in "Linear Method for Determining Monomer Reactivity Ratios in Copolymerization", M. Fineman and S. D. Ross, J. Polymer Science 5, 259 (1950) or "Copolymerization", F. R. Mayo and C. Walling, Chem. Rev. 46, 191 (1950) incorporated herein in its entirety by reference. For example, to determine reactivity ratios the most widely used copolymerization model is based on the following equations:

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$$M_1^* + M_1 = \frac{k_{11}}{k_{12}} M_1^*$$
 (1)
14 $M_1^* + M_2 = \frac{k_{12}}{k_{21}} M_2^*$ (2)
15 $M_2^* + M_1 = \frac{k_{21}}{k_{22}} M_1^*$ (3)
16 $M_2^* + M_2 = \frac{k_{22}}{k_{22}} M_2^*$ (4)

where M_i refers to a monomer molecule which is arbitrarily designated i (where i = 1, 2) and M_2^* refers to a growing polymer chain to which monomer i has most recently attached.

The kij values are the rate constants for the indicated reactions. Thus, k_{11} represents the rate at which an ethylene unit inserts into a growing polymer chain in which the previously inserted monomer unit was also ethylene. The reactivity rates follow as: $r_1=k_{11}/k_{12}$ and $r_2=k_{22}/k_{21}$ wherein k_{11} , k_{12} , k_{22} and k_{21} are the rate constants for ethylene (1) or propylene (2) addition to a catalyst site where the last polymerized monomer is an ethylene (k_{12}) or propylene (k_{22}) .

In Table I the ethylene-propylene reactivity rates r_1 and r_2 are listed for several metallocenes. It can be seen that with increased steric interaction at the monomer coordination site r_1 increases, i.e. the tendency for ethylene polymerization increases over propylene polymerization.

1	It can be seen from Table	I that if one	desires a blend							
2	comprising HDPE/ethylene-prop	ylene copolyme	er one would selec	t						
3.	his/nentamethylcyclopentadien	y])ZrCl ₂ and .								
ن 	historelonentadienvl)Ti diphe	nyl or	PROJECT SHIT							
. 4	dimethyl silvidicyclopentadies	y]:zirconium-	dichloride in raci	DS						
5 6	of 5:1 to 1:1 whe	ereas if one d	esires a blend	3						
6	comprising lippE/ethylene-pro	opylene: one : wo	njq-select#}38							
8	bis(cyclopentadienyl)Zr dime	thyloni25 .36	ecasial religion	z.						
:	bis(methylcyclopentadienyl)Z	rClamand bis(c	yclopentadienyl)T	i :						
9	diphenyl or dimethylsilyldic	yclopentadieny	7 ZrCl ₂ in ratios	· •						
10	of 10:1 to 11:1.	en de de la composition de la composition della composition de la composition de la		<i>:</i>						
11	Desirably, the metalloce	ene molar ratio	will be 10	r:0						
12	a see and proferal	oly 10:1 to -	1:10. The							
13 .	specific metallocenes select	ted and their	molar ratios are							
14	specific metallocenes selection	composition d	esired for the	•						
15	depended upon the molecular composition desired for the component polymers and the overall composition desired for the blend. In general, the component catalyst used in a reactor									
16										
17	blend. In general, the combined blend catalyst mixture will	each have r \	alues which are							
18	blend catalyst mixture will	sind nolum	er compositions W	hich						
19	different in order to produ	ice final poly	let compositions.							
20	comprise blends of two or m	ore polymers.								
21		TABLE I								
		rı	r ₂							
22	Catalyst		.							
			0.0085							
23	Cp2Ti=CH2 Al(Me)2Cl	24	0.015+.002							
24	Cp2TiPh2	19.5+1.5	0.029+.007	•						
25	Me_SiCp_ZrCl2	24+2	0.015+.003							
26	Cp2Zr.Cl2	48+2	0.015005							
27	(Mern) 7rCl	. 60	202.0.007	•						
28	(Me ₅ Cp) ₂ ZrCl ₂	250+30	.002+0.001	······································						
29		50 .	0.007	cvctem						
30	Ti hear stronger used in	the preparation	on of the catalyst	ie						
. 31	i sudrocarhons	n particular	I Man ocar por enes	-						
32	with respect to the	e catalyst sys	Lem. Such Botte	.3 41 E						
33	well known and include, for example, isobutane, butter,									
34	nentane, hexane, heptane, octane, cyclonexane,									
	ALLE AREYORGENEELLA	abuleveloherane toluene, xylene and the like.								

methylcyclohexane, toluene, xylene and the like.

The catalyst systems described herein are suitable for 1 producing polymer product blends in solution, slurry or a gas 2 phase polymerizations and over a wide range of temperatures and 3 pressures. For example, such temperatures may be in the range of -60 to - 280°C and especially in the range of 5 50 to 160 °C. The pressures employed in the process of the present invention are those well known for 7 example, 2 in the range of the late to the second atmospheres and R greater. 9 In a solution phase polymerization the alumoxane and 10

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metallocene can be employed as a homogeneous catalyst system. The alumoxane is preferably dissolved in a suitable solvent, typically in inert hydrocarbon solvent such as toluene, xylene, and the like in molar concentations of 0.1 to 3.0. however greater or lesser amounts can be employed.

The soluble metallocenes can be converted to supported heterogeneous catalyst by depositing said metallocenes on typical catalyst supports such as, for example, silica. alumina, and polyethylene. The solid catalysts in combination with an alumoxane can be usefully employed in slurry and gas phase olefin polymerizations.

After polymerization and deactivation of the catalyst, the product polymer blend can be recovered by processes well known in the art for removal of deactivated catalysts and solution. The solvents may be flashed off from the polymer solution and the polymer obtained extruded into water and cut into pellets or other suitable comminuted shapes.

Pigments, antioxidants and other additives, as is known in the art, may be added to the polymer.

30 The polymer product obtained in accordance with this invention will have a weight average molecular weight in the 500 to . 2,000,000 and preferably 10,000 to range of • 500,000. The component polymers in the reactor blend can have the same or different average molecular weights and comonomer composition; however, it is preferable for most end uses that the average molecular weights and comonomer composition be different.

1 . Illustrative, but nonlimiting examples of reactor blends which can be produced in accordance with this invention are 2 HDPE/EPR copolymer, LLDPE/EPR copolymer, HDPE/LLDPE and 3 -HDPE/LLDPE/EPR copolymer blends. These polymers demonstrate superior properties such as for example impact resistance and tear strength and process more easily than the individual component polymers.

The polymers produced by the process of this present invention are capable of being fabricated into a wide variety of articles, as is known for blend of ethylene and copolymers of ethylene and higher alpha-olefins. The present invention is illustrated by the following examples.

EXAMPLES

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In the examples following the molecular weights were determined on a Water's Associates Model No. 150C GPC. The measurements were made by dissolving polymer samples in hot 17 . trichlorobenzene (TCB) and filtered. The GPC (Gel Permeation Chromotography) runs were performed at 145°C in TCB at 1.5 ml/min using two Shodex A80M/S columns of 9.4 mm internal diameter from Perkins Elmer Inc. 300 milliliter of 3.1 percent solutions in TCB were injected and the chromotographic runs monitored at sensitivity equal -64 and scale factor equal 65. The samples were run in duplicate. The integration parameters were obtained with a Water's Associates data module. An antioxidant, N-phenyl-2-naphthylamine, was added to all samples.

In the examples following the alumoxane was prepared in the following manner:

600cc of a 14.5% solution of trimethylaluminum (TMA) in heptane was added in 30cc increments at 5 minute intervals. with rapid stirring, to 200cc toluene in a Zipperclave reactor under nitrogen and maintained at 100°C. Each increment was immediately followed by the addition of 0.3cc water. The reactor was vented of methane after each addition. Upon completion of the addition, the reactor was stirred for 6 hours while maintaining the temperature at 100°C. The mixture,

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containing soluble alumoxane is allowed to cool to room 1 temperature and settle. The clear solution containing the 2 soluble alumoxane is separated by decantation from the solids. 3 4

Example 1(a) - Reactor blend The effect (the consideration) 5 A 1-liter stainless steel pressure vessel, equipped with an 6 incline blade stirrer, an external water jacket for temperature 7 control, a septum inlet and vent line, and a regulated supply 8 of dry ethylene, propylene and nitrogen, was dried and 9 deoxygenated with a nitrogen flow. 400cc of dry, degassed 10 toluene was introduced directly into the pressure vessel. 25cc 11 of 0.64 molar (in total aluminum) alumoxane was injected into 12 the vessel by a gas tight syringe through the septum inlet and 13 the mixture was stirred at 1,200 rpms and 50°C for 5 minutes 14 at zero (0) psig of nitrogen. 1.12 mg bis(cyclopentadienyl) 15 titanium phenyl dissolved in 2.0 ml of dry, distilled toluene 16 was injected through the septum inlet into the vessel. 17 Similarly, 0.107 mg. bis(pentamethylcylcopentadienyl) zirconium 18 dimethyl in 2.0 ml dry, distilled toluene was injected. The 19 solution was saturated with 200cc propylene at a pressure of 20 165 psig. Thereafter ethylene at 25 psig was passed into the 21 vessel for 60 minutes while maintaining the temperature at 22 50°C at which time the reaction was stopped by rapidly 23 venting and cooling. The copolymer was evaporated to dryness, 24 weighed and analyzed by GPC and IR. 62 gms of a blend of 25 26 polyethylene and EPR copolymer which analyzed for 6 mole % propylene and having a Mn of 16,500 and a Mw of 41,800 was 27 28 recovered.

Example 1(b) - Use of One Metallocene 29 ...

bis(pentamethylcyclopentadienyl)Zirconiumdimethyl 30

A 1-liter stainless steel pressure vessel, equipped with an 31

incline blade stirrer, an external water jacket for temperature 32

control, a septum inlet and vent line, and a regulated supply 33

of dry ethylene, propylene and nitrogen, was dried and 34

deoxygenated with a nitrogen flow. 400cc of dry, degassed 35

toluene was introduced directly into the pressure vessel. 25cc 1 of 0.64 molar (in total aluminum) alumoxane was injected into 2 the vessel by a gas tight syringe through the septum inlet and 3 . the mixture was stirred at 1,200 rpms and 50°C for 5 minutes at zero (0) psig of nitrogen. 0.122 mg bis(pentamethylcyclopentadienyl)zirconium dimethyl dissolved in 2.0 ml of dry, distilled toluene was injected through the septum inlet into the vessel. Liquid propylene (200cc) was : 8 ... added from a calibrated addition vessel resulting in a 9 propylene pressure of 153 psig. Thereafter ethylene at 25 psig 10 was passed into the vessel for 90 minutes while maintaining the 11 temperature at 50°C at which time the reaction was stopped by 12 rapidly venting and cooling. 76 gms of polyethylene which 13 analyzed for 3.4% propylene and having a $\overline{M}n$ of 15,300 and a $\overline{M}w$ 14 of 36,400 was recovered. The analysis was performed as in 15 Example 1(a). 16

Example 1(c) - Use of One Metallocene bis(cyclopentadienyl)Tidiphenyl

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A 1-liter stainless steel pressure vessel, equipped with an incline blade stirrer, an external water jacket for temperature control, a septum inlet and vent line, and a regulated supply of dry ethylene, propylene and nitrogen, was dried and deoxygenated with a nitrogen flow. 400cc of dry, degassed toluene was introduced directly into the pressure vessel. 25cc of 0.64 molar (in total aluminum) alumoxane was injected into the vessel by a gas tight syringe through the septum inlet and the mixture was stirred at 1,200 rpms and 50°C for 5 minutes at zero (0) psig of nitrogen. 1.04 mg bis(cyclopentadienyl) titanium phenyl dissolved in 2.0 ml of dry, distilled toluene was injected through the septum inlet into the vessel. Liquid propylene (200cc) was added from a calibrated addition vessel resulting in a propylene pressure of 165 psig. Thereafter ethylene at 25 psig was passed into the vessel for 90 minutes while maintaining the temperature at 50°C at which time the reaction was stopped by rapidly venting and cooling. 14.4 gms of polyolefin which analyzed for 65% ethylene and 35% propylene and having a Mn of 45,400 and a Mw of 137,000 was recovered.

The analysis was performed as in Example 1(a).

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Example 2 - Use of Two Different Metallocenes

A 1-liter stainless steel pressure vessel, equipped with an incline blade stirrer, an external water jacket for temperature control, a septum inlet and vent line, and a regulated supply of dry ethylene, propylene and nitrogen, was dried and deoxygenated with a nitrogen flow. 400cc of dry, degassed toluene was introduced directly into the pressure vessel. 10.0cc of 0.83 molar (in total aluminum) alumoxane was injected into the vessel by a gas tight syringe through the septum inlet and the mixture was stirred at 1,200 rpms and 80°C for 5 minutes at zero (0) psig of nitrogen. 2.127 mg bis(pentamethylcyclopentadienyl) zirconium dichloride dissolved in 2.0 ml of dry, distilled toluene was injected through the septum inlet into the vessel. Similarly, 0.2628 mg bis(methylcyclopentadienyl) zirconium dichloride in 0.25 ml dry, distilled toluene was injected. The solution was saturated with propylene at a pressure of 111 psig for 15 seconds. Thereafter ethylene at 15 psig was passed into the vessel for 20 minutes while maintaining the temperature at 80°C and the pressure at 126° psig at which time the reaction was stopped by rapidly venting and cooling. 18.0 gms of a blend of PE and EPR copolymer analyzed for 7.1 mole % propylene and having a Mn of 2,000 and a Mw of 8,300 was recovered. A fractionation analysis was performed by stirring a 10 g portion of this solid product for one hour in 100 ml of toluene. The slurry was filtered and washed with 10 ml of fresh toluene. The copolymer in solution and the solid product were separately evaporated to dryness, weighed and analyzed by GPC and IR.

The soluble product (7.0g) had a Mn of 2,200 and a Mw of 11,900 and analyzed for 30 mole % propylene. The insoluble fraction had an Mn of 3000 and a Mw of 7,400 and analyzed to contain 4.8% propylene.

Example 3

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A 1-liter stainless steel pressure vessel, equipped with an incline blade stirrer, an external water jacket for temperature control, a septum inlet and vent line, and a regulated supply of dry ethylene, propylene and nitrogen, was dried and deoxygenated with a nitrogen flow. 400cc of dry, degassed toluene was introduced directly into the pressure vessel. 10cc of alumoxane molar (8.3 m moles in total aluminum) was injected into the vessel by a gas tight syringe through the septum inlet and the mixture was stirred at 1,200 rpms and 50°C for 5 minutes at zero (O) psig of nitrogen. 0.539 mg bis(methylcyclopentadienyl) zirconium dimethyl dissolved in 2.0 ml of dry, distilled toluene was injected through the septum inlet into the vessel. Similarly, 1.03 mg bis(pentamethylcyclopentadienyl) zirconium dichloride in 2.0 ml dry, distilled toluene was injected. The solution was saturated with 200cc propylene at a pressure of 111 psig for 15 seconds. Thereafter ethylene at 25 psig (C_3/C_2) liquid ratio = 16) was passed into the vessel for 20 minutes while maintaining the temperature at 50°C at which time the reaction was stopped by rapidly venting and cooling. 30.0 gms of a blend of LLDPE and EP copolymer analyzed for 3.6% propylene and having a Mn of 5,600 and a Mw of 17,300 was recovered. The fractionation analysis, GPC & IR performed as in Example 2 yielded 3.0 gms of a soluble fraction having a $\overline{\text{M}}\text{n}$ of 3,500, a Mw of 16,000 and mole % of C_3^{\pm} of 20.6. The insoluble fraction (7.0 gms) had a Mn of 5,400, a Mw of 16,400 and mole % C_3^{\pm} of 2.9%.

CLAIMS:

- 1. A catalyst system for the production of reactor blend polymers, said catalyst comprising (a) at least two different organometallic coordination compounds which are derivatives of mono, di or tricyclopentadienyls with Group 4b, 5b and 6b transition metal, the compounds having different reactivity with respect to the monomers employed and (b) an alumoxane.
- 2. A homogeneous catalyst system for the production of reactor blend polymers comprising a blend of polyethylene and an ethylene-olefin copolymer; said catalyst comprising:
 - (a) at least two metallocenes having represented by the general formula (C₅R')_pR''_s(C₅R'_m)MeQ_{3-p} or R''_s(C₅R'_m)₂MeQ' each having different reactivity ratios, and
 - wherein $(C_5R'_m)$ is a cyclopentadienyl or substituted cyclopentadienyl, each R' which can be the same or different is hydrogen or a hydrocarbyl radical or two R' substituents together form a fused C_4 - C_6 ring, R" is a C_1 - C_4 alkylene radical, a dialkyl germanium or silicone, or an alkyl phosphine or amine radical bridging two $(C_5R'_m)$ rings, Q is a hydrocarbon radical or halogen and can be the same or different, Q' is an alkylidene radical having from 1 to 20 carbon atoms, Me is a transition metal of Group 4b, 5b and 6b, s is 0 or 1, p is 0, 1 or 2; when p = 0, s = 0; m is 4 when s is 1; m is 5 when s is 0.
- 3. The catalyst system of claim 2 wherein Q is methyl, phenyl or chloride.

- 4. The catalyst system of claim 2 or claim 3, wherein Me is selected from zirconium and titanium.
- 5. The catalyst system of claim 4 comprising at least 2 zirconocenes.
- 6. The catalyst system of claim 4 comprising at least 1 titanocene and 1 zirconocene.
- 7. The catalyst system of claim 5 comprising bis (methylcyclopentadienyl) zirconium dichloride and bis (pentamethylcyclopentadienyl) zirconium dichloride.
- 8. A process for producing a reactor blend comprising polymerizing ethylene and at least alpha-olefin simultaneously in the presence of the catalyst system of any of claims 1 to 7.
- 9. The process of claim 8 wherein the polymer blend comprises a blend of polyethylene and copolyethylene-propylene.
- 10. The process of claim 9 wherein the polyethylene is LLDPE or HDPE.



EUROPEAN SEARCH REPORT

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Application number

EP 84 30 3806

DOCUMENTS CONSIDERED TO BE RELEVANT						· . ·
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